State University of New York

# EECE 301 <br> Signals \& Systems Prof. Mark Fowler 

Note Set \#10

- C-T Signals: Circuits with Periodic Sources


## Solving Circuits with Periodic Sources

FS makes it easy to find the response of an RLC circuit to a periodic source!

- Use the FS to convert the source into a sum of sinusoids
- Do phasor analysis for each of the input sinusoids (think superposition!)
- Add up the sinusoidal responses to get the output signal

Example: In electronics you have seen (or will see) how to use diodes and an RC filter circuit to create a DC power supply:

Obviously we can't do this for all infinitely many terms.. but we can do it for enough... and if we do it numerically it is not hard!


## Progression of Ideas



For this scenario we can find the $c_{k}$ analytically...
The equation for the FS coefficients is: $\quad c_{k}=\frac{1}{T} \int_{0}^{T} x(t) e^{-j k \omega_{0} t} d t \quad \omega_{0}=\frac{2 \pi}{T}$


Change of variable: $\tau=\frac{\pi}{T} t \quad \square c_{k}=\frac{A}{\pi} \int_{0}^{\pi} \sin (\tau) e^{-j k 2 \tau} d \tau$
Use a Table of Integrals and do some algebra \& trig to get:

$$
c_{k}=\frac{2 A}{\pi\left(1-4 k^{2}\right)}
$$

FS coefficient for full-wave rectified sine wave of amplitude A

## So the two-sided spectrum after the rectifier:



Now we can us Parseval's Theorem to determine how many terms we need in our approximation for the source...

$$
\begin{aligned}
& P=\frac{1}{T} \int_{0}^{T} A^{2} \sin ^{2}\left(\frac{\pi}{T} t\right) d t=\frac{A^{2}}{\pi} \int_{0}^{\pi} \sin ^{2}(\tau) d \tau=\frac{A^{2}}{\pi} \frac{\pi}{2}=\frac{A^{2}}{2} \\
& P_{\text {approx }}=\sum_{k=-K}^{K}\left|c_{k}\right|^{2}=\sum_{k=-K}^{K}\left|\frac{2 A}{\pi\left(1-4 k^{2}\right)}\right|^{2}=\frac{4 A^{2}}{\pi^{2}} \sum_{k=-K}^{K}\left|\frac{1}{\left(1-4 k^{2}\right)}\right|^{2}
\end{aligned}
$$

We can look at the ratio of these two as a good measure:

$$
\frac{P_{\text {approx }}}{P}=\frac{\frac{4 A^{2}}{\pi^{2}} \sum_{k=-K}^{K}\left|\frac{1}{\left(1-4 k^{2}\right)}\right|^{2}}{\frac{A^{2}}{2}}=\frac{8}{\pi^{2}} \sum_{k=-K}^{K}\left|\frac{1}{\left(1-4 k^{2}\right)}\right|^{2}
$$

Numerically evaluating this for different $K$ values shows that $K=10$ retains more than $99.99 \%$ of the power. So we can use that value.

So... our numerical approach is now this:

1. Numerically evaluate $c_{k}$ for $\mathrm{k}=-10$ to 10
2. Numerically convert them into the $d_{k}$ phasors
3. Convert the phasors into corresponding FS

$$
\begin{aligned}
& c_{k}=\frac{2 A}{\pi\left(1-4 k^{2}\right)} \\
& d_{k}=\left[\frac{1}{1+j k \omega_{o} R C}\right] c_{k}
\end{aligned}
$$ sinusoidal terms and add them up

We'll do this for:

- $A=10$ volts

- $R=100 \Omega$
- $C=1000 \mu \mathrm{~F}$
wo $=240^{*} \mathrm{pi} ; \%$ Set fund freq
fo=wo/(2*pi); \% convert to Hz
$\mathrm{T}=2^{*} \mathrm{pi} / \mathrm{wo}$; \% compute period
$\mathrm{K}=10$; \% Set number of terms
$\mathrm{kv}=(-\mathrm{K}): \mathrm{K}$; \% set vector of k indices
$\mathrm{A}=10$; \% set amplitude of input
$\mathrm{R}=100$; \% set resistance
C=1000e-6; \% set capacitance
$\mathrm{ck}=\left(2^{*} \mathrm{~A} / \mathrm{pi}\right) . /\left(1-4^{*}(\mathrm{kv} . \wedge 2)\right) ; \%$ compute the input FS coefficents
$\mathrm{dk}=\left(1 . /\left(1+\mathrm{j} * \mathrm{kv}^{*} \mathrm{wo}{ }^{*} \mathrm{R} * \mathrm{C}\right)\right) . * \mathrm{ck} ; \%$ compute the output FS coefficents
Fs $=4 * \mathrm{~K} * \mathrm{fo} ; \quad \%$ Compute sampling rate (set here to twice the minimum value of 2 Kfo )
$\mathrm{Ts}=1 / \mathrm{Fs} ; \quad \%$ Compute sample spacing
$\mathrm{t}=\left(-3^{*} \mathrm{~T}\right): \mathrm{Ts}:(3 * \mathrm{~T})$;
x_apprx = zeros(size(t)); \% sets up vector of zeros as first "partial sum"
for $\mathrm{k}=(-\mathrm{K}): \mathrm{K} \quad \%$ loop through "all" coefficients
x_apprx $=x \_a p p r x+c k(k+K+1) * \exp \left(j^{*} k^{*} w^{*}{ }^{*} t\right) ; \quad \%$ Add current term to partial sum
end
x_apprx = real(x_apprx);
y_apprx = zeros(size(t)); \% sets up vector of zeros as first "partial sum"
for $\mathrm{k}=(-\mathrm{K}): \mathrm{K} \quad$ \% loop through "all" coefficients
y_apprx $=y \_$apprx $+\mathrm{dk}(\mathrm{k}+\mathrm{K}+1)^{*} \exp \left(\mathrm{j}^{*} \mathrm{k}^{*} \mathrm{wo} \mathrm{o}^{*} \mathrm{t}\right) ; \quad \%$ Add current term to partial sum
end
y_apprx $=$ real(y_apprx); \% theory says imaginary parts cancel.. . so enforce this in case $\%$ of numerical round-off issues
figure(1); plot(t,x_apprx,'r',t,y_apprx,'g--'); xlabel('time (seconds)'); ylabel('Input and Output (volts)'); grid figure(2); subplot(2,1,1); stem(kv,abs(ck)); subplot(2,1,2); stem(kv,abs(dk))




## Big Idea: "Frequency Response"



How to find the Frequency Response of a Circuit...

- Assume arbitrary phasor $X$ with frequency $\omega$
- Analyze circuit to find output phasor $Y$
- It will always take this multiplicative form: $Y=H(\omega) X$
- All impedances are evaluated at the arbitrary frequency $\omega$
- The frequency response function $H(\omega)$ is the thing that multiplies $X$

